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## On The Performance of Imt-2000 Communication Link Based on Stratospheric Platforms


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## ON THE PERFORMANCE OF IMT-2000 COMMUNICATION LINK BASED ON STRATOSPHERIC PLATFORMS

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### Abstract

A new means for providing wireless communication has been currently proposed. It is based on aerial vehicle known as High Altitude Platform or Stratospheric Platforms (SPF). The SPF will be operated at an altitude of 17-22 km above the ground. Therefore, the channel condition may be different compared with those of the conventional terrestrial or satellite wireless channel. In this paper, the channel propagation characteristic of such a system is firstly investigated by means of ray tracing algorithm. We emphasize our investigation in a typical urban environment, in which the mobile users mostly exist. We developed building block model for simulation based on building height distribution, which is obtained from measurement inside Tokyo. As a result, propagation loss model and Ricean channel parameter for the SPF channel is reported in different scenarios. By using this result we then estimate the required transmitted power of SPF to serve the mobile users in a several transmission rate that is used in IMT-2000 services. Finally, an evaluation of BER of IMT-2000 link is performed in order to estimate the system level performance. From this evaluation, the main contribution of this paper is to clearly show the critical limitations of both power requirement as well as system level performance of mobile communication IMT-2000 by using the concept of the SPF.

*Keywords: link performance, IMT-2000, high altitude platform, stratospheric platform*

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### 1. Introduction

The increasing demand of high-capacity wireless services has led the rapid deployment of wireless communication infrastructure, especially for delivery at remote area. Currently, we have two well-established methods for providing wireless services those are terrestrial and satellite systems. In terrestrial system, a huge number of base stations have to be deployed for the need of line of sight propagation path. While in satellite system the problem is capacity limitation. In recent year, another alternative has been attracting much the attention of providing wireless services. It is based on an unmanned or manned airship or aircraft that is called High Altitude Platform Station (HAPS) or known by different names as Stratospheric Platform (SPF) [1-4]. They will be located at stratosphere in the altitude of around 17-22 km above the ground. This altitude has not been used for telecommunication services except perhaps for the use related to scientific re-search. Air stream in this altitude is relatively calm and therefore it is a fairly niche area to put the communication facilities onboard the platform.

SPF has the capability to combine the best features of the conventional terrestrial and satellite system. For example, a wider coverage area compared with the terrestrial system but lower power requirement and propagation delay compared with the satellite system. The most important advantages of SPF systems are their easy and incremental deployment, flexible and reconfigurable, low-cost operation, high elevation angles, broad coverage, broadband capability, ability to move around in emergency situation, etc. With those excellent features of SPF, ITU has allocated spectrum to this system in a several frequency band. Those are in the bands of 48/47 GHz world wide, 31/28 GHz for the use mostly in Asia country, and bands of 2 GHz for the use of 3G and beyond 3G.

There are three categories of SPF technology are now being proposed and classified broadly as: an unmanned airship with propulsion system, a solar unmanned aircraft, and a manned aircraft [5]. Research and development related to the SPF communication and technology has been started over the last few years in several countries all over the world. In Japan, NICT has

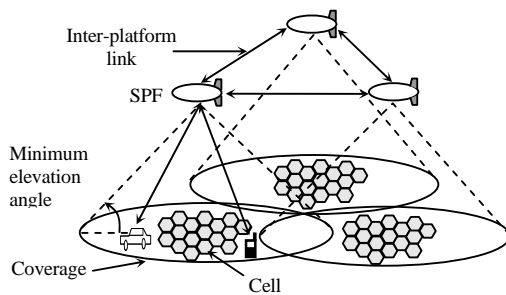


Figure 1. SPF Configuration for IMT-2000

taken an initiative and responsibility of a national R&D SPF project since 1998 [6]. The similar ongoing project has also been undertaken in the European countries through the CAPANINA project [7], in the U.S. they have the Aerovironment/Sky-Tower project [8], and also the stratospheric platforms program in Korea with KARI/ETRI [9-10]. Those investigations are indeed devoted to put the SPF into operation for the new wireless infrastructure.

The most promising applications that can be carried out by the SPF system are cellular telephony, broadband local multipoint distribution system (LMDS) services, and access provision to digital networks (internet, ISDN). From the geometrical features of the system, SPF is designed to have the capability to deliver high quality digital video, TV broadcasting, as well as a remote sensing and navigation system.

The basic cellular configuration of SPF for IMT-2000 is depicted in Figure 1. A single platform is able to cover a large area within a radius of 50-200 km, depending upon the minimum elevation angle and frequency. Furthermore, inter platform optical link provides a gigabit data rate transmission. Therefore, multiple platforms can be arranged in the sky in order to increase the capacity or to extend the coverage area. As a result, all wireless communication toward the end users can be realized by this system without installing many base stations. This appealing system is therefore expected to be the new wireless infrastructure in the near future.

As the work was progressing in development of such a system, one aspect that has not been much investigated is propagation characteristics of its link. We know that the propagation characteristic in SPF mobile communication system is a complicated process that involves multiple reflections, diffraction, or scattering. The simplified model of propagation mechanism can be depicted such as in Figure 2. Specific research to the

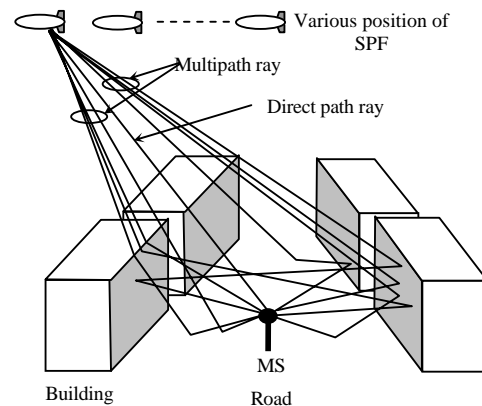


Figure 2. Multipath in a SPF channel

small scale propagation modeling for SPF channel is introduced in [11]. However the model doesn't analyze the impact of elevation and azimuth angle, in which the SPF is seen by the mobile station (MS). In our previous work, we have performed the performance evaluation and the channel characterization for SPF system based upon the measurement with considering the impact of elevation angle [12,13]. We found that the platform channel is Ricean distributed and the performance of the channel is an increasing function to the elevation angle. On the other hand, the SPF is a power limited system. Thus, while the platform is now being developed, an estimation to the required transmitted power onboard the platform is considered as a matter of urgency. Therefore, in this paper, a ray tracing based propagation loss model, power requirement estimation, and system level performance evaluation of communication link are demonstrated in order to estimate the possibility of using SPF for IMT-2000 services.

## 2. Method of Experiment

In case of SPF with high elevation angle, propagation path is mostly characterized as having line of sight (LOS). In this case, many number of SPF are required to cover global coverage. By contrary, when SPF is deployed with low elevation angle to extend the coverage for example, propagation path will suffer from non-line of sight (NLOS) situation. It then results the increasing propagation loss especially for the user located near the edge of the coverage. To show the propagation environment of SPF communication link, an extensive series of field experiments are performed inside and nearby the city of Tokyo, Japan. The model configuration of our experiment is depicted in Figure 3 and Figure 4 for side view and top view, respectively.

The experiments have two main targets. First target is to find the average building height and the result is demonstrated in Table 1. In the table, we observed that

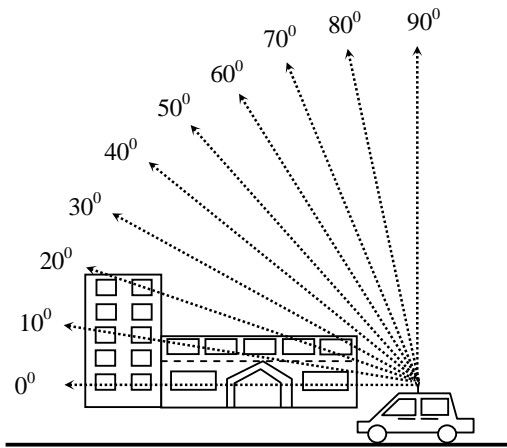


Figure 3. Side view (elevation angle variation)

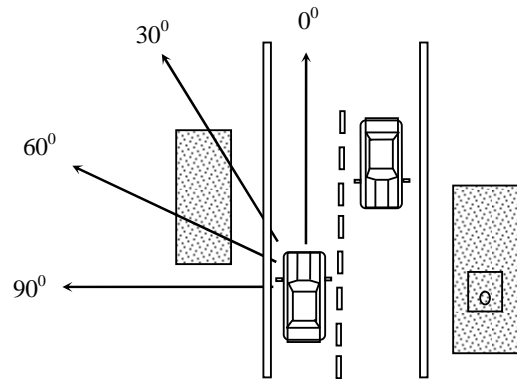


Figure 4. Top view (azimuth angle variation)

Table 1. Average building height and density

Area	Average building height [m]	Building density [pieces/km <sup>2</sup> ]
Shinjuku	25.5	290
Shibuya	25.0	200
Asakusa	22.1	580
Kiryu	19.1	7

in Shinjuku, an average building height is found to be the highest and followed by that in Shibuya, Asakusa, and Kiryu. In the table, we also observed building density in pieces/km<sup>2</sup>. We found the highest building density is in Asakusa and followed by that in Shinjuku, Shibuya, and Kiryu. From this geographical data, we then develop the model of urban environment for propagation evaluation that will be presented in the next section of this paper.

The second target of our survey is to estimate visibility. The visibility is defined as the probability at each elevation angle that the MS looking at the SPF without shadowed by the building. The experiment is carried out by driving a car which is equipped with a video camera. Our car was moved the various directions in the city for about 5 km in total. As we know that the propagation attenuation will increase when the link is shadowed by the building or structure. We performed in the survey four different azimuth angles (i.e. 0°, 30°, 60°, and 90°) while elevation angle is measured from 10° to 80° in a step of 10°. Elevation angle is defined as in Figure 3 while azimuth angle is a relative angle with respect to the street direction such as described in Figure 4. Result of visibility in Asakusa area is demonstrated in Figure 5.

The markers (triangles, diamonds, squares, and circles) demonstrate the result of experiments, and the lines (solid, dashed, dotted, and dashed-dot) illustrate an approximation of the visibility derived by mathematical expression. Mathematical empirical model for visibility for the data of Asakusa area can be expressed as a function of elevation ( $\alpha$ ) and azimuth ( $\theta$ ) angle by the following equation

$$p_v(\alpha, \theta) = \begin{cases} (\sin \alpha)^{0.01} & ; \theta = 0^\circ \\ (\sin \alpha)^{\sin \theta} & ; \theta = 30^\circ, 60^\circ, 90^\circ \end{cases} \quad (1)$$

where  $\theta=0^\circ$  is in a positive y-axis direction and  $\theta=90^\circ$  is in a negative x-axis direction as explained in Figure 6. Bold solid line in Figure 5 is a theoretical Rayleigh distribution model for the visibility. We found from our survey, the visibility curve of azimuth 30°, 60°, and 90° have a good agreement with the Rayleigh curve. It means that the visibility for those azimuth angles can be modeled by Rayleigh distribution.

We developed building block model that represents an urban environment for propagation evaluation. It then followed by examination of ray tracing algorithm,

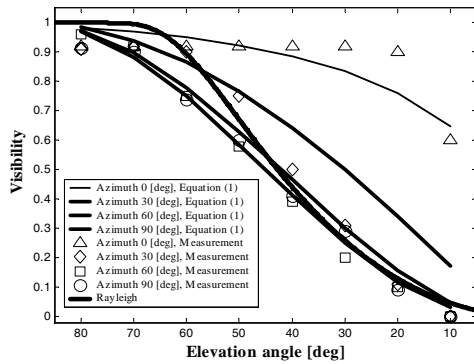


Figure 5. Visibility in Asakusa

which is applied to the developed building block model for simulation. Building block model we developed in this paper is an approaching model to the result of our experiments. We developed the model for the block of 12 buildings over the area of  $0.0451 \text{ km}^2$  ( $205 \text{ m} \times 220 \text{ m}$ ) and is depicted in Figure 6. It means the building density of our model is  $266 \text{ pieces/km}^2$ . For a simplification of using ray tracing algorithm, we assume all the buildings under test have equal height of  $20 \text{ m}$ . Therefore, if we refer to the result of experiment, our building block model is a representation of urban environment characteristic between Asakusa and Kiryu area in the sense of average building height. These areas have a characteristic with a high-rise building representing one of the most metropolitan cities.

In the model, the SPF elevation angle is made to vary from  $5^\circ$  to  $90^\circ$  to provide a complete model of propagation evaluation for this system. Meanwhile, three scenarios of the SPF position that is seen by the MS are considered. Those are azimuth angle ( $\theta$ ) of  $90^\circ$ ,  $60^\circ$  and  $30^\circ$  in order to observe different direction of propagation path between the SPF and the MS. The MS is positioned in the center of the street (point A) assuming the user is in a vehicle in the road. Table 2 is a summary of geometrical parameters involved in the ray tracing simulation.

Ray tracing tool we developed follows an approach model proposed by Tila [14]. But in our model, we included diffraction mechanism effects from building rooftops. This mechanism occurs when a large object such as a building obstructs the radio path, causing the waves to be bended into shadow region and continue to propagate toward the receiver. It is therefore found to be

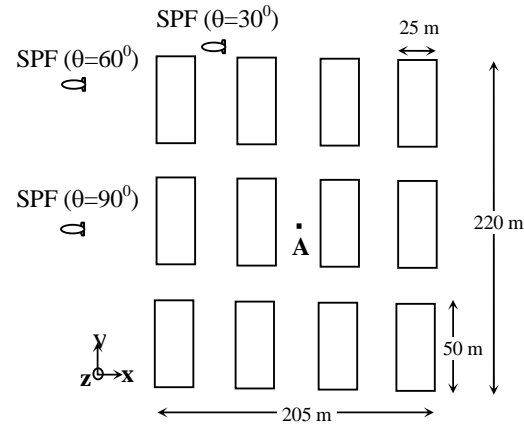


Figure 6. Top view of the model

important to include diffraction in ray tracing algorithm, especially in case of SPF with low elevation angle. The model employs a number of virtual transmitters as depicted in Figure 7. They are located around the area under test in order to overcome the difficulty of applying the ray launching methods for the large separation such as from the SPF to the MS. The generation of virtual transmitters is repeated when the elevation angle has to be changed in the simulation. Note in this paper we examined various elevation angles from  $5^\circ$  to  $90^\circ$ .

We employ nine categories of ray to be included in our simulation. These ray categories are line of sight, single reflection from building, single reflection from street, double reflection from building to street, double reflection from building to building, diffraction from rooftop of building, diffraction from rooftop and single reflection from building, diffraction from rooftop and single reflection from street, and diffraction from rooftop and double reflection from building to street. Rays outside the above categories are assumed to leave the target and terminated from the simulation environment.

We assume the following electrical parameters throughout the prediction in this paper. Buildings are assumed to be made of concrete with  $\epsilon_r = 3$  and  $\sigma = 0.005 \Omega^{-1}m^{-1}$ , while the ground is modeled as having  $\epsilon_r = 15$  and  $\sigma = 7 \Omega^{-1}m^{-1}$  [15], where  $\epsilon_r$  and  $\sigma$  are dielectric constant and conductivity, respectively. In the prediction, two situations were observed, those are LOS situation and shadow situation (when direct ray is obstructed by the building nearby the MS).

Table 2. Geometrical parameters

Parameters	Specification
SPF height (h)	20 km
Frequency (f)	2 GHz
Building height ( $h_b$ )	20 m
Building width ( $w_b$ )	25 m
Building length ( $w_l$ )	50 m
Street width ( $w_s$ )	35 m
MS antenna height ( $h_m$ )	1.5 m
SPF elevation ( $\alpha$ )	$5^\circ$ to $90^\circ$ (step $1^\circ$ )
SPF azimuth ( $\theta$ )	$90^\circ$ , $60^\circ$ and $30^\circ$

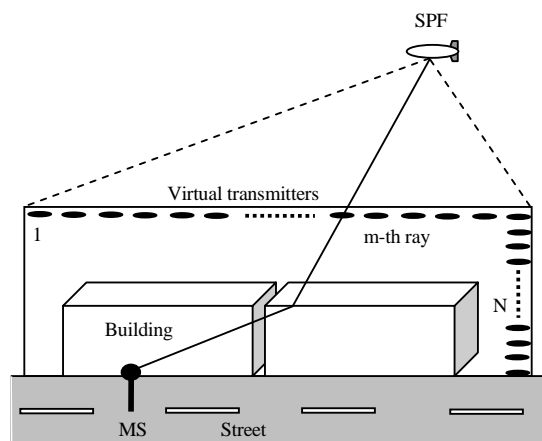


Figure 7. Concept of virtual transmitters [14]

Ray tracing algorithm requires firstly searching rays and secondly computing electromagnetic field of each ray. The basic idea in ray tracing is to employ a geometrical optic (GO) and uniform theory of diffraction (UTD). UTD is an extension method of GO to include diffraction [16].

Basic principle of GO is a Snellius's law of reflection as depicted in Figure 8. By using ray tracing algorithm, we are able to search the reflection rays until they reach the receiver. In this work we consider up to two reflections either by the building surface, the street or their combination. Diffraction principle as described in Figure 9 is applied in our simulation. Rays undergo diffraction by rooftop edge of the building and continue up to two reflections are also considered in the simulation.

Both transmitting (SPF) and receiving (MS) antennas are assumed to be an isotropic with a 0 dB gain. Therefore, an electric fields of ray arriving at the receiving antenna for direct ray ( $E_{LOS}$ ), reflected ray ( $E_R$ )

and diffracted ray ( $E_D$ ), respectively are calculated using the following formulas

$$E_{LOS} = E_0 \frac{e^{-j\beta d_0}}{d_0} \quad (2)$$

$$E_R = E_0 \cdot \bar{R} \frac{e^{-j\beta(s_1+s_2)}}{s_1+s_2} \quad (3)$$

$$E_D = \frac{E_0}{s'} \cdot \bar{D} \sqrt{\frac{s_3}{s(s+s_3)}} e^{-j\beta(s+s_3)} \quad (4)$$

where  $\beta = \lambda/2\pi$  is propagation constant,  $E_0$  is emitted electric field from transmitter,  $d_0$  is direct path length,  $s_1$  is path length from the source to reflection point,  $s_2$  is path length from reflection point to the receiver,  $s$  is path length from the source to diffraction point, and  $s_3$  is path length from diffraction point to receiver.  $\bar{R}$  is a Fresnel dyadic reflection coefficient and  $\bar{D}$  is dyadic finite conductivity edge diffraction coefficient. These two coefficients follow the general formulation

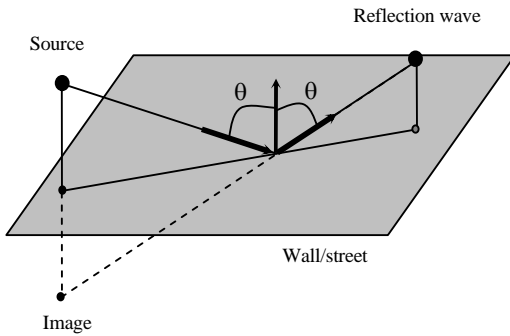


Figure 8. Reflection mechanism

presented by Bertoni [15]. Finally, respective rays for each ray category were added at the MS and expressed as

$$E_i = \sum_{j=1}^n E_j \quad (5)$$

$E_j$  is the received electric field of the  $j$ -th ray for  $i$ th category. Note we assume that the ray tracing algorithm employed in this work consider up to nine categories of ray as mentioned above. Although the precision can be improved by additional ray category such as double diffraction in combination with multiple reflection from wall and street, however we have to compensate by computational complexity and therefore it actually time consuming. Generally, rays after second reflection will have very weak power. In this work, the total electric field contribution consists of vector summation of nine ray categories and can be expressed by

$$E_{Tot} = \sum_{i=1}^9 E_i \quad (6)$$

Finally, the total path loss ( $L$ ) can be given by

$$L = 20 \log \left( \frac{\lambda}{4\pi} \frac{|E_{Tot}|}{|E_0|} \right) \quad (7)$$

From equation (7), now we are able to demonstrate the propagation path loss for the above-mentioned model as a function of elevation and azimuth angle, which is presented in the following section.

### 3. Result and Discussion

Figure 10 exhibits the ray-tracing simulation result of a total propagation loss obtained from the calculation of a direct LOS ray and multipath scattered rays. In a figure,

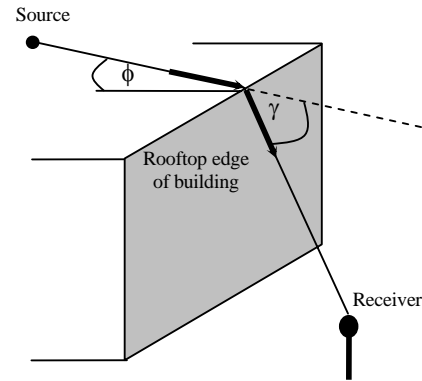


Figure 9. Diffraction mechanism

we can see the propagation loss in a LOS situation for three kinds of azimuth angle ( $90^\circ$ ,  $60^\circ$ , and  $30^\circ$ ) are exactly similar along with elevation angle variation. However in a NLOS situation, different azimuth angle exhibits different value of propagation loss. This is due to the contribution of the rays is different for different azimuth angle. In azimuth angle of  $90^\circ$ , the propagation loss shows to be the largest and decreases as azimuth angle also decreases. We observe in NLOS situation, the propagation loss dramatically increases by the order of 20 dB or more compared to that in LOS region. In this case we can evaluate that the propagation loss in the SPF communication is less sensitive concerning to the azimuth angle in case of high elevation angle. By contrary, in low elevation angle or particularly in the shadow region, the propagation loss is dependent and quite sensitive to the azimuth angle.

We are also able to obtain  $K$  factor from our ray tracing simulation result. The  $K$  factor is a Ricean distribution parameter that indicates the ratio between a direct ray power and the multipath power. In this paper, we directly get the  $K$  factor value by using the following expression

$$K = \frac{A^2}{2\sigma^2} \quad (8)$$

where  $A$  represents the amplitude of direct LOS ray or dominant ray and  $\sigma^2$  is the variance or average power of the multipath components. Since there is no direct ray in NLOS region,  $K$  factor goes to zero in this region, for example in low elevation angle. It is shown in Figure 11, there is a transition region between LOS and NLOS region (ranging from  $36^\circ$  up to  $46^\circ$  of elevation angle for all azimuth angle),  $K$  factor is gradually increased due to the presence of direct ray. From these results, it is obvious that the MS may be fail to establish the communication link with the SPF either due to a very

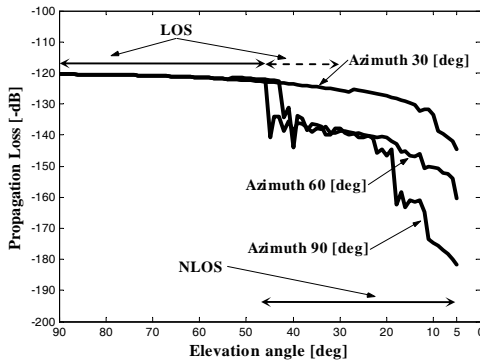


Figure 10. Predicted propagation loss for the model shown in Figure 6

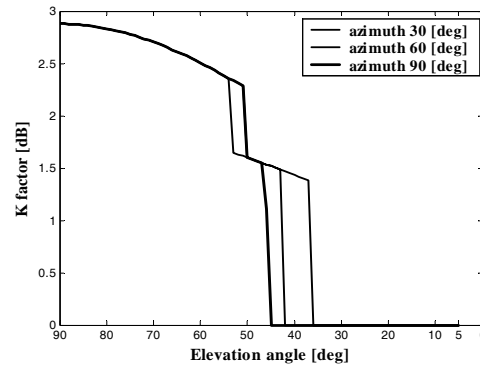


Figure 11. K factor

Table 3. IMT-2000 specifications for SPF [19]

Item	Specification
Frequency [GHz]	2
Bit rate [kbps]	8, 32, 64, 384, and 2000
SPF antenna gain [dBi]	30
MS antenna gain [dBi]	0
Boltzmann's constant [J/K]	$1.38 \times 10^{-23}$
Temperature's chamber [K]	290
Link margin [dB]	15.4
Cable, connector, and other losses [dB]	2
$E_b/N_0$ [dB]	Max. 7.9

high propagation loss or very poor condition of the channel performance indicated by a very low value of  $K$  factor

One of the proposed services in SPF communication is the next generation of mobile communication IMT-2000 [17]. In this paper, we present an analysis of required transmit power for such a system. For digital CDMA-based such as IMT-2000, the required bit energy per noise power spectral density ( $E_b/N_0$ ) can be expressed by the following simple formulation [18]

$$\frac{E_b}{N_0} = \frac{P_T G_T G_R}{R_b k T_0 L(\alpha, \theta) L_0 M_L} \quad (9)$$

- $P_T$  : SPF power transmit
- $G_T$  : SPF antenna gain
- $G_R$  : MS antenna gain
- $R_b$  : Bit rate
- $k$  : Boltzmann's constant ( $1.38 \times 10^{-23} \text{ m}^2 \text{ kg s}^{-2} \text{ K}^{-1}$ )
- $T_0$  : Receiver temperature
- $L(\alpha, \theta)$ : Propagation loss obtained in Fig. 10
- $L_0$  : Cable, connector, and combiner loss
- $M_L$  : Link margin

We employ the standard specifications that are used for IMT-2000 services, which are described in Table 3 in order to estimate the required transmit power by the SPF. The purpose of this estimation is to observe the capability of SPF, which is regarded as a power limited system in order to deliver mobile services to the users. Propagation simulation result in Figure 10 therefore needs to be used to achieve this goal. Since IMT-2000 provides various applications (i.e. voice, data, multimedia, and internet), it is important to consider bit rate in the evaluation of required transmit power.

Results are shown in Figure 12 (a), (b) and (c) for the scenarios of azimuth 90°, 60° and 30°, respectively. A very critical required transmit power occurs at elevation angle below 10° in a scenario azimuth angle of 90°, even for a very low information rate (8 kbps). For that case, the required transmit power would vary between 31.2 W (8 kbps) and 7.80 kW (2 Mbps) for a single carrier. Such high values may be impractical. However, for elevation angle greater than 10°, the required transmit power for low to medium information rate (i.e. 8 kbps up to 384 kbps) is fairly low so that the SPF system is possible to deliver IMT-2000 services in all azimuth angle scenarios. In a LOS region such as elevation angle greater than 60°, in the sense of power requirement, the



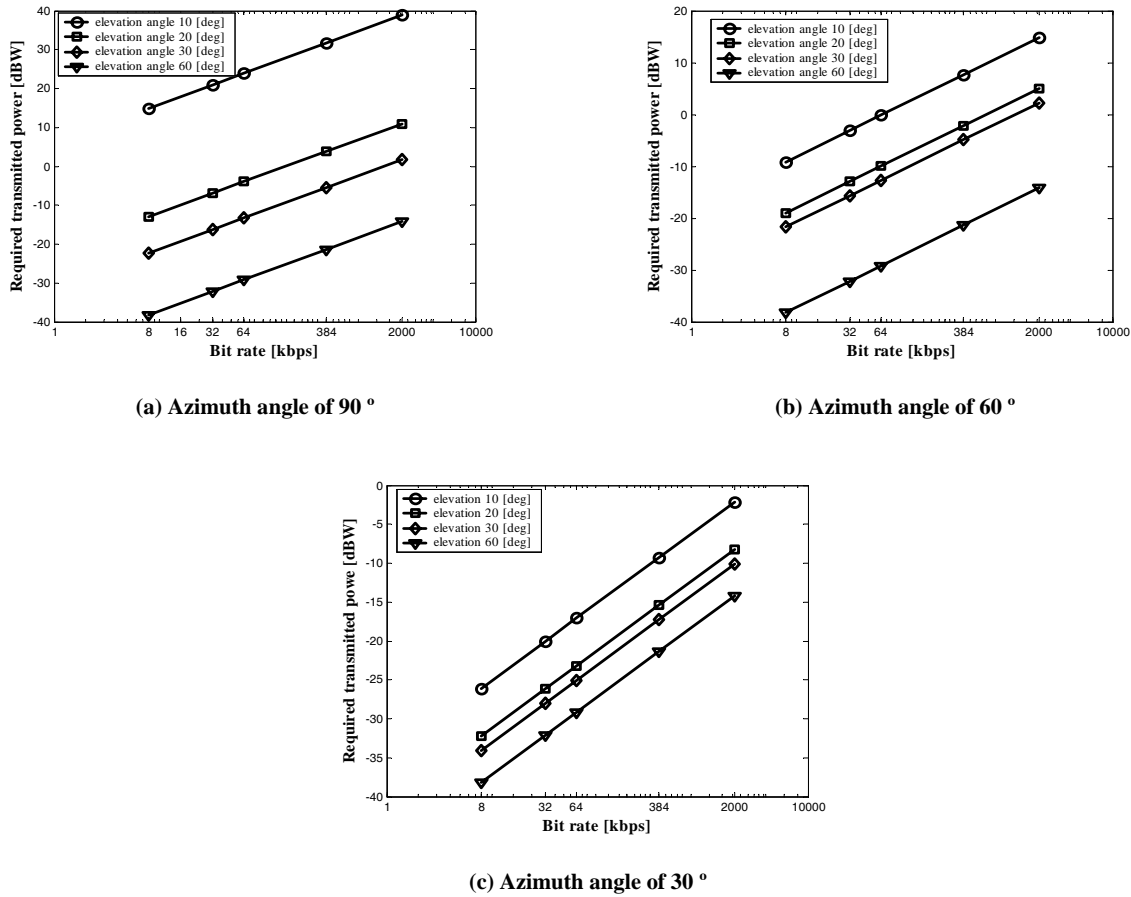


Figure 12. Required transmitted power at the SPF

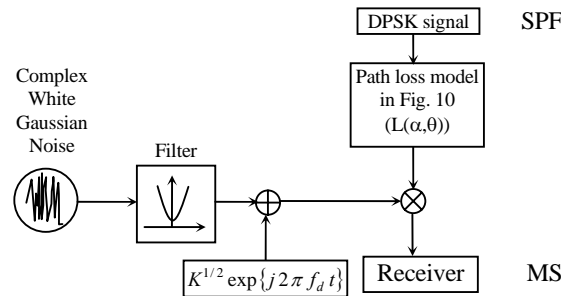


Figure 13. The model of SPF channel

SPF is convinced to have the capability of delivering IMT-2000 services for bit rate up to 2 Mbps

We have analyzed the propagation loss and the required transmit power, however, in order to provide a complete evaluation we have to observe the BER performance of IMT-2000 link served by the SPF. Based on previous analysis of  $K$  factor, it is shown that the channel of SPF is characterized with two types of distribution. Those

are Ricean distributed for LOS situation and Rayleigh distributed ( $K$  equals 0) for NLOS situation. Considering those channel distribution at an appropriate elevation angle (indicated by  $K$  factor in Figure 11), we then evaluate BER performance. The model for BER simulation is shown in Figure 13. We employ DPSK modulation scheme and frequency slow and flat channel model in the evaluation. The latter assumption is based on a consideration that the coherence time of the

channel is larger than the symbol period and the coherence bandwidth of the channel is greater than the bandwidth of the signal. Although the delay profile of a real measurement result for a case of SPF is unavailable so far, the model proposed by DAVIS et. al. [11] shows a good approach to the SPF channel. For DPSK modulation scheme under such fading channel condition, the closed form solution of bit error probability can be expressed by [18],

$$P_{e,DPSK} = \frac{(1+K)}{2(\Gamma+1+K)} \exp\left(-\frac{K\Gamma}{\Gamma+1+K}\right) \quad (10)$$

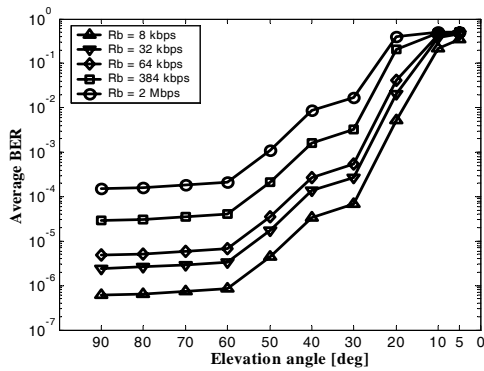
where  $\Gamma = \overline{\beta^2} E_b / N_0$  is the average value of the signal to noise ratio,  $\overline{\beta^2}$  is unit variance of amplitude values of the fading channel, and  $K$  is the Rice factor.

In Figure 14, we demonstrate average BER evaluation result for azimuth angle of 90°, 60° and 30°. The bit rate carried out by IMT-2000 is considered up to 2 Mbps. From the result, we can see that the link performance in 90° azimuth angle is the worst case, while in 30° azimuth

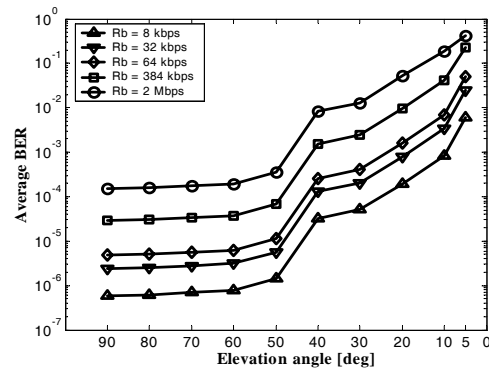
angle is the best case. In 90° of azimuth angle, the performance decreases quickly when the link is NLOS. We also observed the performance in low elevation angle such as lower than 30°, to achieve BER equals or lower than 10<sup>-3</sup>; it is only possible if the bit rate is lower than 384 kbps for all azimuth angles. On the other hand, in LOS situation such as in elevation angle greater than 45°, it is shown an error floor in the BER curves due to the presence of multipath components. Therefore, SPF link would require multipath mitigation techniques to improve link quality.

### 4. Conclusion

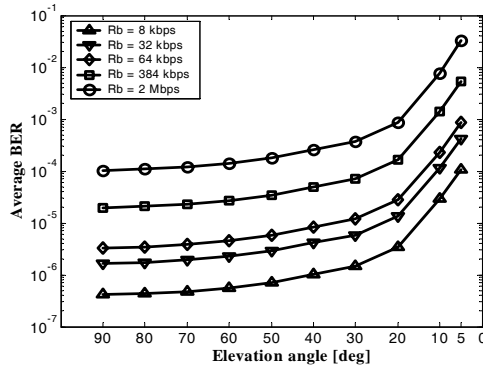
This paper has presented and demonstrated the ray tracing algorithm to examine the performance of IMT-2000 communication link that is carried out by a new wireless media that is called the SPF. Specific model of urban environment was first developed based on the measurement data that was carried out inside and around Tokyo city for examination. Results of examination have clearly shown the channel model of the SPF mobile link. Two parameters were obtained



(a) Azimuth angle of 90 °



(b) Azimuth angle of 60 °



(c) Azimuth angle of 30 °

Figure 14. Performance of IMT-2000 link in SPF channel

from simulation. Those are propagation loss and Rice factor for different azimuth angle in a wide range of elevation angle. We found in general, propagation loss is a decreasing function of elevation angle. However, when elevation angle is decreasing, shadowing from building has led the propagation loss to dramatically increase by a value of 20 dB or more. Azimuth angles have also important contribution especially in the region of low elevation angle. For azimuth  $90^\circ$ , the critical required transmit power in the model is observed for elevation angle below  $20^\circ$ . Such required power may be too high in the implementation of SPF mobile communication. Finally, we demonstrate the BER performance for SPF IMT-2000 mobile link. Generally, the SPF link performance gets worse in low elevation angle. However, link performance is also influenced by azimuth angle. It means the orientation of the user toward the SPF is also important. The performance is intolerable even in the lowest bit rate of IMT-2000 services (8 kbps) when a user is in the position of  $90^\circ$  of azimuth and elevation lower than  $20^\circ$ . It is because the shadowing attenuation due to building was too high. Therefore, the critical limitation of choosing the minimum elevation angle in the application of IMT-2000 based on SPF has been clearly shown in this paper.

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